## EXPLANATION OF SETBACK AND GREEN AREA MEASUREMENTS

Although the Applicant is seeking relief from the rear yard and side yard requirements, many of the buildings in the project plan have adjacent open space which meets or exceeds the yard requirements in the Zoning Regulations. For example, the rear and side yards of Building 1 technically do not meet the Zoning Regulations if the yards are measured to the theoretical lot lines. However, the open space between the rear yard of this building and the project's property line is uninterrupted. From the rear of this building to the property line, the project provides approximately 35 feet of open space, which effectively extends the rear yard well in excess of that required in the Zoning Regulations. Further, the northern side of the building has a de facto extended side yard because of the uninterrupted open space between the side of the building and the project property line.

In total, at least 16 buildings $^{1}$ in the project have some uninterrupted open space between their side and/or rear yards and the project property line. This situation effectively provides greater rear and/or side yards for many of the buildings in the project despite the smaller legal size of these yards for which the Applicant is seeking variance relief. If the Zoning Commission considers these "extended" yards on many of the buildings, therı the amount of rear/side yard variance relief for the project is considerably smaller.

[^0]|  |  | Side Yard Setback |  |  |  |  | Rear Yard Setback |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bldg \# | Front Provided ^ |  | Controlling <br> Lot \#"ms | $\begin{array}{\|c} \text { Bldg } \\ \text { height at } \\ \text { Side } \end{array}$ | Required | Provided ^ | Controlling Lot\# | $\begin{array}{c\|} \text { Bldg } \\ \text { height at } \\ \text { Rear } \end{array}$ | Required | Provided* |
| 1 | 34.6 | R | 7 | 41.70 | 13.90 | 1.5**** | 7 | 42.80 | 15.0 | 13.0 |
|  |  | L | 1 | 42.83 | NA ${ }^{\text {a** }}$ | NA | 7 | 42.80 | 15.0 | 13.0 |
| 2 | 7.0 | R | 8 | 43.00 | $\mathrm{NA}^{\text {N"M }}$ | NA | 14 | 44.80 | 15.0 | 13.0 |
|  |  | L | 14 | 43.00 | 14.30 | $\frac{1.5}{1.5 \times \ldots}$ |  |  |  |  |
| 3 | 7.0 | L | 15 | 43.67 | $\mathrm{NA}^{\text {ºm }}$ | NA | 15 | 42.27 | 15.0 | 13.0 |
| 4 | 7.0 | R | 22 | 43.80 | NA ${ }^{\text {+2* }}$ | NA |  |  |  |  |
|  |  | L | 28 | 44.33 | 14.78 | $1.5{ }^{\text {mamm }}$ | 22 | 44.60 | 15.0 | 13.0 |
| 5 | 7.0 | R | 35 | 45.67 | 15.22 | 1.5 "mom | 29 | 42.20 | 15.0 | 13.0 |
|  |  | L | 29 | 43.00 | NA ${ }^{\text {+N\% }}$ | NA | 29 | 42.20 | 15.0 | 13.0 |
| 6 | 7.0 | R | 36 | 43.67 | NA ${ }^{\text {ma** }}$ | NA | 36 | 44.77 | 15.0 | 13.0 |
|  |  | L | 43 | 43.67 | 14.56 | 12.5 |  |  |  |  |
| 7 | 7.0 | R | 50 | 42.83 | 14.28 | 12.5 | 44 | 41.90 | 15.0 | 13.0 |
|  |  | L | 44 | 42.50 | NA ${ }^{\text {²* }}$ | NA | 44 | 41.90 | 15.0 | 13.0 |
| 8 | 20.2 | R | 51 | 42.63 | NA ${ }^{\text {+K* }}$ | NA | 51 | 44.73 | 15.0 | 13.0 |
|  |  | L | 57 | 43.17 | 14.39 | 12.5 |  |  |  |  |
| 9** | 27.6* | R | 62 | 49.83 | $\mathrm{NA}^{\text {+2* }}$ | NA | 58 | 51.40 | 16.9 | 13.0 |
|  |  | L | 58 | 54.50 | $\mathrm{NA}^{* * *}$ | NA |  | 5.40 | 16.9 | 13.0 |
| 10 | 7.0 | R | 63 | 47.33 | $\mathrm{NA}^{\text {+4* }}$ | NA | 67 | 42.90 | 15.0 | 13.0 |
|  |  | L | 67 | 42.00 | $N A^{\text {TF }}$ | NA |  |  |  |  |
| 11 | 7.0 | R | 75 | 48.19 | 16.06 | 43.2 | 75 | 52.59 | 17.5 | 13.0 |
|  |  | L | 68 | 50.52 | $\mathrm{NA}^{\text {"** }}$ | NA |  | 52.59 | 17.5 | 13.0 |
| 12 | 7.0 | R | 76 | 44.00 | NA"** | NA | 76 | 42.50 | 15.0 | 13.0 |
|  |  | L | 78 | 41.67 | 13.89 | 2.6 |  |  |  |  |
| 13 | 7.0 | R | 88 | 49.52 50.19 | $\frac{16.51}{\text { NA }{ }^{\text {m* }}}$ | 2.6 | 86 | 52.19 | 17.3 | 13.0 |
|  |  | L | 86 | 50.19 | NA ${ }^{* * *}$ | NA | 86 | 52.15 |  | 13.0 |
| 14 | 10.0 | R | 79 | 43.33 | $\mathrm{NA}^{* * *}$ | NA | 79 | 44.43 | 15.0 | 13.0 |
|  |  | L | 85 | 44.00 | NA*** | NA |  |  |  |  |
| 15 | 10.5 | R | 96 | 47.52 | $\mathrm{NA}^{* * *}$ | NA | 106 | 52.26 | 17.4 | 13.0 |
| 16 | 25.7* | R | 89 | 43.33 | NA"** | NA | 89 | 35.00 | 15.0 | 13.0 |
|  |  | L | 95 | 43.00 | 14.33 | 2.6 |  |  |  |  |
| 17 | $33.4 *$ | R | 115 | 42.17 | 14.06 | 2.6 | 107 | 44.00 | 15.0 | 13.0 |
|  |  | L | 107 | 43.00 | NA"** | NA | 107 | 44.00 | 15.0 |  |
| 18 | 14.1 | R | 116 | 44.50 | $\mathrm{NA}^{\text {+4* }}$ | NA | 124 | 42.50 | 15.0 | 13.0 |
|  |  | L | 124 | 43.50 | 14.50 | 2.6 |  |  |  |  |


|  |  | Side Yard Setback |  |  |  |  | Rear Yard Setback |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Bldg \# }}{19}$ | $\begin{array}{\|c\|} \text { Front } \\ \text { Provided A } \\ \hline \end{array}$ |  | Controlling Lot \#**** | $\begin{array}{\|c\|} \begin{array}{c} \text { lidg } \\ \text { height at } \\ \text { Side } \end{array} \\ \hline \end{array}$ | Required | Provided $\wedge$ | Controlling | $\begin{array}{\|c\|} \hline \text { Bldg } \\ \text { height at } \\ \text { Rear } \end{array}$ | Required | Provided* |
|  | 7.0 | R | 129 | 53.39 | 17.80 | 14.5 | 125 | 51.92 | 17.3 | 13.0 |
|  |  | L | 125 | 50.02 | NA ${ }^{\text {T* }}$ | NA |  |  |  |  |
| 20 | 7.0 | I | 130 | 43.67 | $\mathrm{NA}^{\text {™ }}$ | NA |  |  |  | 13.0 |
|  |  | L | 134 | 50.03 | 16.68 | 14.5 | 130 | 42.07 | 15.0 |  |
| 21 | 7.0 | R | 139 | 51.17 | 17.06 | 14.5 | 135 | 43.90 | 15.0 | 13.0 |
|  |  | L | 135 | 42.50 | NA ${ }^{\text {+4* }}$ | N ${ }^{\text {a }}$. |  |  |  |  |
| 22 | 7.0 | R | 140 | 42.50 | $\mathrm{NA}^{\text {™ }}$ | NA |  |  |  | 13.0 |
|  |  | L | 144 | 51.17 | 17.06 | 14.5 | 144 | 44.37 | 15.0 |  |
| 23 | 7.0 | R | 149 | 48.50 | 16.17 | 14.5 | 145 | 42.00 | 15.0 | 13.0 |
|  |  | L | 145 | 43.50 | NA ${ }^{\text {+ }}$ | NA |  |  |  |  |
| 24 | 7.0 | R | 150 | 48.86 | NA ${ }^{\text {"*P }}$ | NA | 150 | 52.06 | 17.3 | 13.0 |
|  | $34.4 *$ | $\frac{L}{R}$ | 154 | 51.33 45.17 | 17.11 | 14.5 10.5 | 150 | 52.06 | 17.3 |  |
| 25 |  | L | 155 | 42.67 | ${ }^{\text {NA }}{ }^{\text {™ }}$ | N ${ }^{\text {a }}$ | 155 | 42.87 | 15.0 | 13.0 |
| 26 | 39.0 * | R | 168 | 47.19 | 15.73 | 4.6 |  |  |  | 13.0 |
|  |  | L | 161 | 50.19 | NA ${ }^{\text {"** }}$ | N/2. | 161 | 52.39 | 17.5 |  |
| 27 | $39.0{ }^{*}$ | R | 173 | 48.86 | ${ }_{\text {NA }}{ }^{\text {ant }}$ | N/ | 173 | 52.46 | 17.5 | 13.0 |
|  |  | L | 169 | 50.19 | 16.73 | 4.6 |  |  |  |  |
| $28^{*+}$ | 34.5* | R | 179 | 56.52 | 18.84 | 4.6 | 179 | 59.82 | 19.6 | 13.0 |
|  |  | L | 174 | 56.19 | NA*** | NA. | 179 | 59.82 | 19.6 |  |
| 29** | $34.5 *$ | R | 185 | 56.86 | $\frac{N A^{\text {TK }}}{}$ | $\mathrm{N}^{\text {K }}$ | 185 | 59.36 | 19.8 | 13.0 |
|  |  | L | 180 | 55.52 | 18.51 | 4.6 | 18 | 59.36 | 19.8 |  |
| 30 | 18.3 | R | 186 | 41.93 | $\mathrm{NA}^{+\underline{+4}}$ | $\mathrm{N} \cdot$ | 191 | 42.70 | 15.0 | 13.0 |
|  |  | L | 191 | 42.00 | 14.00 | 2.6 | 191 | 42.70 | 15.0 |  |
| 31 | 5.0 | R | 192 | 42.67 | NA ${ }^{\text {+4* }}$ | $\mathrm{N}_{4}$ | 198 | 42.63 | 15.0 | 13.0 |
|  |  | L | 198 | 42.63 | 14.21 | 14.3 |  |  |  |  |
| 32 | $32.2^{*}$ | R | 199 | 43.00 | 14.33 | 11.5 | 209 | 42.73 | 15.0 | 13.0 |
|  |  | L | 209 | 41.63 | 13.88 | 2.6 | 209 | 42.73 | 15.0 |  |
| 33 | 11.3 | R | 218 | 43.00 | 14.33 | 16.5 | 210 | 44.67 | 15.0 | 13.0 |
|  |  | L | 210 | 44.67 | NA ${ }^{\text {™ }}$ | NA |  |  |  |  |
| 34 | 7.0 | R | 219 | 44.00 | NA ${ }^{\text {™ }}$ | NA | 228 | 42.00 | 15.0 | 13.0 |
|  |  | L | 228 | 42.00 | 14.00 | 31.7 | 228 | 42.00 | 15.0 | 13.0 |
| 35 | 7.0 | R | 235 | 43.67 | 14.56 | 13.7 | 235 | 43.87 | 15.0 | 13.0 |
|  |  | L | 229 | 42.67 | NA ${ }^{\text {²* }}$ | NA |  |  |  |  |
| 36 | 29.5* | $\frac{\mathrm{R}}{\mathrm{L}}$ | 236 | 42.50 | $\stackrel{N A}{ }{ }^{\text {an** }}$ | $\frac{\mathrm{N} / 4}{6.7}$ | 237 | 42.50 | 15.0 | 13.0 |
|  |  | L | 237 | 42.50 | 14.17 | 6.7 |  |  |  |  |

Noies. Measured to Center of Alliey or Pivivate Street
** Buildings 9,28 and 29 will have a peaked roof (LFF to highest point of roof $=48.0$ feet); all other buildings will have flat roots (LFF to highest point of roof $=41.0$ )
** NA = None required, considered comer lo
...2 Side setback direction detemined from facing front of building
$\wedge$ All setbacks shown provided in this chart have been reduced 0.5 feet from that shown in plan to allow for variance in thickness of exterior wall treatment





[^0]:    ${ }^{1}$ Buildings $1,6,7,8,18,19,20,21,22,23,24,25,33,34,35,36$

